CAEE 211 Geology Laboratory 6 Lab Date: 29 July 2016



## **Rock Mechanics and Seismology Laboratory**

Due Date: 5 August 2016 Attendance (based on signing): 30 points

Submitting Student Name: \_\_\_\_\_

Members of laboratory group (no more than three):

#### **Rock Mechanics**

1) During a site investigation, a boring was advanced to a depth of 30 ft (9.1 m) at which point rock was encountered. The ground water table (GWT) was encountered at 30 ft (9.1m), the depth of rock, during the investigation. The engineering geologist decided to advance the boring into the rock by drilling to a depth of 16.4 ft (5 m). The recovered rock cores were positioned in a rock core box from top down as shown in Figure 1. The beginning of the rock core was located in the upper left hand corner of the box and each following piece of the core was placed from left to right on each row with increasing depth. Each row of the rock core box represents a depth of the 3.2 ft (1 m) of drilling depth, therefore the total drill depth that can be contained in the box is 16.4 ft (5 m)



**Figure 1** – Recovered Rock Cores

Using Figure 1 determine the amount of recovered rock in pieces of 10 cm or longer in length. Determine the Rock Quality Designation (RQD) for the recovered rock cores using Equation 1. Using Table 7.7 provide a description of rock quality.

# $RQD = \frac{\sum of \ the \ rock \ core \ lengths \ greater \ the \ 10 \ cm}{\sum of \ the \ total \ drill \ depth} \ x \ 100\% \ \dots \ Eq \ 1$

Total Amount of Recovered Rock = (ft) (m)

RQD = \_\_\_\_\_

Table 7.7 Rock	(Quality Designation (RQD)		
RQD (%)	Description of Rock Quality		
0–25	Very poor		
25-50	Poor		
50-75	Fair		
75-90	Good		
90-100	Excellent		

Description of Rock Quality = \_\_\_\_\_

2) The profile of the soil stratum was developed from the boring during the site investigation is shown in Figure 2. Calculate the existing vertical stress ( $\sigma_v$ ) on the rock bed (at a depth of 30 ft) using Equation 2:

$\sigma_v = \gamma_a n_a + \gamma_b n_b + \gamma_c n_c \dots Eq$
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Figure 2 – Soil Profile

Existing Vertical Stress ( $\sigma_v$ ) = \_\_\_\_\_ (psf) \_\_\_\_\_ (kg/cm<sup>2</sup>)

3) From the recovered rock cores, two unconfined compression tests were conducted on test specimens, which were 2 in. in diameter and 4 in. long. The load verses displacement data for the two tests are presented in Tables 1 (sandstone) and 2 (gneiss).

Table 2 – Unconfined Compression Data

for Gneiss

Axial	Compressive	Axial	Compressive
Deformation (in)	Load (lb)	Deformation (in)	Load (lb)
0	0	(	0
0.0012	3140	0.001332	7534.964
0.0024	6280	0.002664	15069.93
0.0044	12560	0.004884	30139.86
0.0064	18840	0.007104	45209.78
0.0084	25120	0.009324	60279.71
0.0112	31400	0.012432	75349.64
0.0144	32970	0.015984	79117.12
0.016	31400	0.01776	75349.64

 
 Table 1 – Unconfined Compression Data for Sandstone

Develop the compressive stress ( $\sigma_a$  in psi) verses axial strain ( $\epsilon$  in in. /in.) plots for both tests using equations 3, 4 and 5. Present these plots in the same graph for comparison. Determine the ultimate unconfined compressive strength ( $\sigma_a$ ) for each rock type. Calculate the Modulus of Elasticity ( $E_{t50}$ ) at 50% of  $\sigma_a$  using the corresponding strain at 50% of  $\sigma_a$  and Modulus Ratio ( $M_r$ ) for each rock type using equations 6 and 7. Using Tables 7.3, 7.4, and Figure 7.28 to determine the Strength Classification of the Intact Rock, the Modulus of Elasticity Classification of the Intact Rock and plot the  $M_r$  for each rock type.

$$Area = \pi r^{2} \dots Eq 3$$

$$\sigma_{a} = \frac{Force}{Area} \dots Eq 4$$

$$\in = \frac{change \ in \ length}{initial \ length} \dots Eq 5$$

$$E_{t50} = \frac{\sigma_{a} \ 50\%}{\epsilon} \dots Eq 6$$

$$M_{r} = E_{t50} / \sigma_{a} \dots Eq 7$$

Unconfined Compressive strength ( $\sigma_a$ ) of sandstone = \_\_\_\_ (psi) \_\_\_\_ (kg/cm<sup>2</sup>)

Unconfined Compressive strength ( $\sigma_a$ ) of gneiss = \_\_\_\_ (psi) \_\_\_\_ (kg/cm<sup>2</sup>)

Modulus of Elasticity ( $E_{t50}$ ) of sandstone = \_\_\_\_\_ (psi) \_\_\_\_\_ (kg/cm<sup>2</sup>)

Modulus of Elasticity ( $E_{t50}$ ) of gneiss = \_\_\_\_ (psi) \_\_\_\_ (kg/cm<sup>2</sup>)

Modulus Ratio  $(M_r)$  of sandstone = \_\_\_\_\_

Modulus Ratio  $(M_r)$  of gneiss = \_\_\_\_\_

Do the Modulus Ratios correlate well with respective figures in your textbook for the rock types?

~		Unconfined Compressive	Description	$E_{t_{50}}(\mathrm{kg/cm^2} imes10^5)$
Class	Description	Strength (kg/cm²)	Very stiff	8-16
Δ	Very high strongth	>2250	Stiff	4-8
B	High strongth	1125-2250	Medium stiffness	2–4
C	Medium strength	562-1125	Low stiffness	1-2
D	Low strength	281-562	Yielding	0.5-1
E	Very low strength	<281	Highly yielding	0.25-0.5

Strength Classification of the Intact Rock of sandstone =

Strength Classification of the Intact Rock of gneiss =

Modulus of Elasticity Classification of the Intact Rock of sandstone = \_\_\_\_

Modulus of Elasticity Classification of the Intact Rock of gneiss =



4) Additional triaxial testing was conducted on the gneiss. Three triaxial tests were performed on intact specimens of the gneiss at confining pressures of 1000, 2000, and 3000 psi (70.3, 140.4, and 210.9 kg/cm<sup>2</sup>). The test data for the three triaxial tests are presented in Figure 3.



Figure 3 – Triaxial Compression Tests on Intact Specimens of Gneiss

Develop the Mohr Circles for each of the three tests using equations 8, 9 and 10. Determine the cohesion (c) and friction angle ( $\Phi$ ) that best fits the test data for the gneiss as defined by equation 11.

 $\sigma_3 = minor \ principal \ stress \ ... \ Eq \ 8$  $\sigma_1 = major \ principal \ stress = \ \sigma_3 + \Delta P \ ... \ Eq \ 9$  $\Delta P = deviator \ stress \ ... \ Eq \ 10$  $\tau = c + \ \sigma \tan \Phi \ ... \ Eq \ 11$ 

Cohesion (C) of gneiss = \_\_\_\_\_ (psi) \_\_\_\_\_ (kg/cm<sup>2</sup>)

Friction Angle ( $\Phi$ ) of gneiss = \_\_\_\_ (°)

Using equation 12 calculate the unconfined compressive strength ( $\sigma_a$ ) for the gneiss.

$$\sigma_a = 2 C \tan (45 + \frac{\phi}{2}) \dots Eq 12$$

Unconfined compressive strength ( $\sigma_a$ ) of gneiss = \_\_\_\_\_ (psi) \_\_\_\_\_ (kg/cm<sup>2</sup>)

How does this  $\sigma_a$  compare to the actual unconfined compression test on the gneiss?

Knowing that the tensile strength of rock is typically 5 to 10% of  $\sigma_a$ , estimate the tensile strength (T<sub>0</sub>) of the gneiss.

Tensile strength (T<sub>0</sub>) of gneiss = \_\_\_\_\_ (psi) \_\_\_\_\_ (kg/cm<sup>2</sup>)

5) Using the an RQD value calculated from Part 1 and the Unconfined Compressive Strength determined from Part 3 for the gneiss determine the Rock Mass Rating (RMR) for a tunnel which is to be excavated 50 ft (15.2 m) below the ground surface in the bedrock using the following information. The spacing of the discontinuities were found to be 380 mm apart and consisted of slightly weathered, slightly rough surfaces separated by less 1mm. The rock mass inflow per 10 m of tunnel length was observed to be approximately 70 liter/minute, with considerable outwash of joint fillings. The strike parallel to the tunnel axis had a dip of 35°. Provide the Rock Mass Rating, Class Number, Description, and Meaning of Rock Mass Class using the Tables 7.8 and 7.9 provided in the Appendix.

Rock Mass Rating = \_\_\_\_\_

Class Number = \_\_\_\_\_

Description = \_\_\_\_\_

Provide the meaning of the Rock Mass Class with regard to stand-up time, cohesion and friction angle of the rock mass.

### Seismology

We will be using a "virtual" seismogram laboratory developed at UCLA for this lab. Go to this website:

http://www.sciencecourseware.com/virtualearthquake/VQuakeExecute.html?x=131&y=80 to get started.

This page has additional explanations and tutorials if you run into a snag: http://www.sciencecourseware.org/eec/earthquake/

The USGS has an interactive website that discusses the 1906 San Francisco EQ. You can import a few files into Google Earth and look at historic pictures of the earthquakes. It is really neat! <u>http://earthquake.usgs.gov/earthquakes/</u>

#### Assignment/Questions

- 1. What is a seismic wave?
- 2. What are the two types of seismic waves that seismologists use? Describe each type of wave and the differences between them.

- 3. What earthquake did you select?
- 4. Do a screen capture or cut and paste the following results:

a) Comparison of your location of the Epicenter to the actual location of the Epicenter with the summary table of the results.

b) The Richter's nomogram with your estimated magnitude.

c) Virtual Seismologist Certificate of Completion showing your finalized tabulated results. Please do not e-mail a certificate to the instructor (5 points OFF if you do!!!).

5. Answer problems 13, 14, 15, 16 and 17 from Chapter 8 from the Kehew textbook.

### APPENDIX

A	CLASSIEICA	TION PARAMETERS A	ND THEIR RATING	CS				
-	. CLASSIFICA	I ION FARAMETERS A	VD THEIR RATIN	33		n (111		
	Pai	rameter				Range of Values		
Strength of intact rock Point-load strength index (MPa)		>10	4-10	2–4	1–2	For this low range uniaxial compressiv test is preferred		
l	mineral	Uniaxial compressive strength (MPa)	>250	100-250	50-100	25-50	5-25 1	I-5 ·
		Rating	15	12	7	4	2	1
Drill core quality RQD (%) Rating		90-100	75-90	50-75	25~50	<25		
		20	17	13	8	3		
	Spacing	of discontinuities	>2 m	0.6–2 m	200-600 mm	60-200 mm	<60 mm	
		Rating	20	15	10	8	5	
Condition of discontinuities		Very rough surfaces Not continuous No separation Unweathered wall rock	Slightly rough surfaces Separation <1 mm Slightly weathered walls	Slightly rough surfaces Separation <1 mm Highly weathered walls	Slickensided surfaces or Gouge <5 mm thick or Separation 1-5 mm Continuous	Soft gouge >5 mm thick or Separation >5 mm Continuous		
		Rating	30	25	20	10	(	)
		Inflow per 10 m tunnel length (L/min)	None	<10	10-25	25-125	>1	25
	3	419 1000	– or –	- or	- or	- or	- or	
5	Groundwater	Ratio Joint water pressure Major principal stress	0	<0.1	0.1-0.2	0.2-0.5	>(	0.5
		General conditions	Completely dry	Damp	Wet	Dripping	Flow	ving
Rating		15	10	7	4	(	)	
3	RATING AD	USTMENT FOR DISCO	NTINUITY ORIEN	TATIONS				
	Par	rameter			Range of Values			
Strike and dip orientations of discontinuities		Very Favorable	Favorable	Fair	Unfavorable	Very Unf	avorable	
		funnels and mines	0	-2	-5	-10	-1	12
R	tatings	Foundations	0	-2	-7	-15	-2	25
		Slopes	0	-5	-25	-50	-6	50
	ROCK MASS	CLASSES DETERMINI	ED FROM TOTAL I	RATINGS				
	R	ating	100-81	80-61	60-41	40-21	<	20
	Cl	are no	1	n	m	N/	N	,
	Des	cription	Very good rock	Good rock	Fair rock	Poor rock	Very po	or rock
			nay good total				seed by	
Ľ	). MEANING C	JF ROCK MASS CLASS	15					27
Class no. Average stand-up time		1 20 yr for 15-m	1 yr for 10-m	1 wk for 5-m	10 h for 2.5-m	30 min 1	for 1-m	
	Cohorion of th	io mark mare (kPa)	span	span 200.400	span 200.200	span 100.200	spa	aut
	Conesion of th	te rock mass (kPa)	>400	300-400	200-300	100-200	<100	
	menon angle of	the rock mass (deg)	56 T 16	<ul> <li>Control (Section 2018) Section</li> </ul>	<ul> <li>International Control of Contro</li></ul>			

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Table 7.9 Effe	ct of Discontinuity St	rike and Dip Or	ientations in Tunneling
Strike Perpendicul Drive wi	ar to Tunnel Axis ith Dip	D	rive against Dip
Dip 45-90	Dip 20-45	Dip 45-90	Dip 20-45
Very favorable	Favorable	Fair	Unfavorable
Strike Parallel t	o Tunnel Axis		Irrespective of Strike
Dip 20-45 Dip 45-90			Dip 0-20
Fair Very unfavorable			Fair

Source: Z. T. Bieniawski, Engineering Rock Mass Classifications, New York, Wiley Interscience, © 1989.